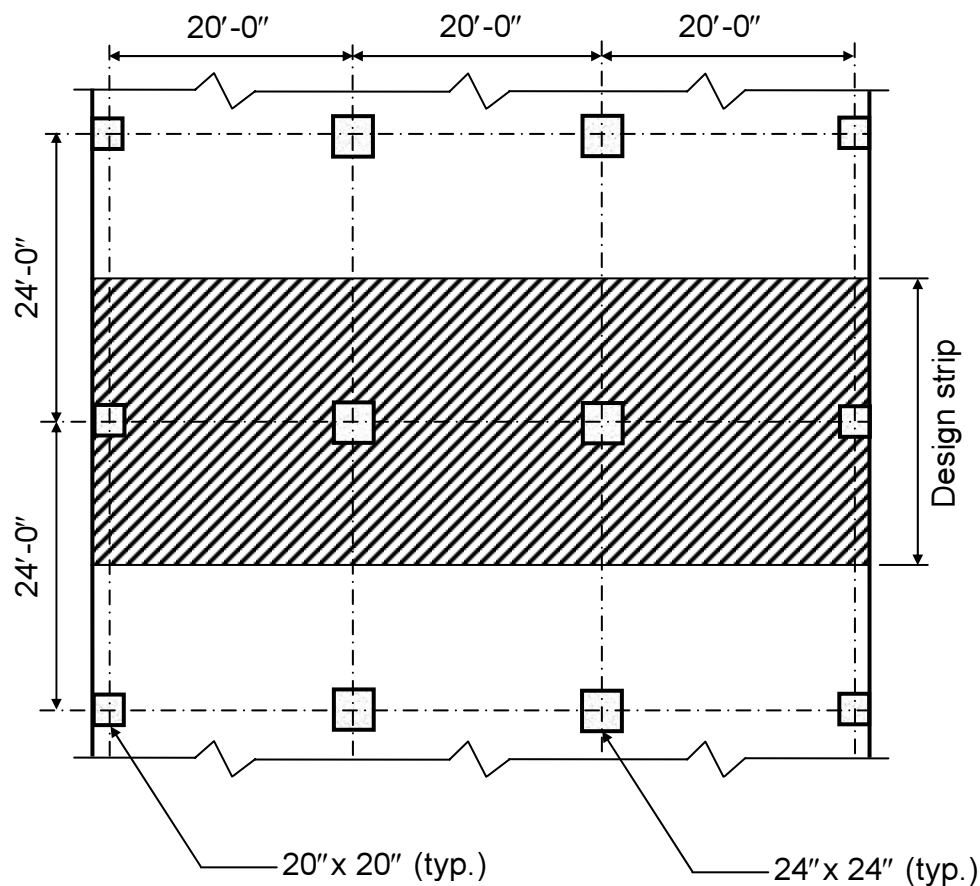


Two-Way Slabs

The following example illustrates the design methods presented in the PCA book "Simplified Design - Reinforced Concrete Buildings of Moderate Size and Height" third edition. Unless otherwise noted, all referenced table, figure, and equation numbers are from that book.

Example Building

Below is a partial plan of a typical floor in a cast-in-place reinforced concrete building. In this example, an interior strip of a flat plate floor system is designed and detailed for the effects of gravity loads according to ACI 318-05.



Design Data

Materials

- Concrete: normal weight (150 pcf), $3/4$ -in. maximum aggregate, $f'_c = 4,000$ psi
- Mild reinforcing steel: Grade 60 ($f_y = 60,000$ psi)

Loads

- Superimposed dead loads = 30 psf
- Live load = 50 psf

Two-Way Slabs

Minimum Slab Thickness

Longest clear span $\ell_n = 24 - (20/12) = 22.33$ ft

From Fig. 4-3, minimum thickness h per ACI Table 9.5(c) = $\ell_n/30 = 8.9$ in.

Use Fig. 1-8 to determine h based on shear requirements at interior column assuming a 9 in. slab:

$$q_u = 1.2(112.5 + 30) + 1.6(50) = 251.0 \text{ psf}$$

$$A = 24 \times 20 = 480 \text{ ft}^2$$

$$A/c_1^2 = 480/2^2 = 120$$

From Fig. 1-8, $d/c_1 \approx 0.22$

$$d = 0.22 \times 24 = 5.3 \text{ in.}$$

$$h = 5.3 + 1.25 = 6.55 \text{ in.}$$

Try preliminary $h = 9$ in.

Design for Flexure

Use Fig. 4-4 to determine if the Direct Design Method of ACI Sect. 13.6 can be utilized to compute the bending moments due to the gravity loads:

- 3 continuous spans in one direction, more than 3 in the other O.K.
- Rectangular panels with long-to-short span ratio = $24/20 = 1.2 < 2$ O.K.
- Successive span lengths in each direction are equal O.K.
- No offset columns O.K.
- $L/D = 50/(112.5 + 30) = 0.35 < 2$ O.K.
- Slab system has no beams N.A.

Since all requirements are satisfied, the Direct Design Method can be used.

Total panel moment M_o in end span:

$$M_o = \frac{q_u \ell_2 \ell_n^2}{8} = \frac{0.251 \times 24 \times 18.167^2}{8} = 248.5 \text{ ft-kips}$$

Total panel moment M_o in interior span:

$$M_o = \frac{q_u \ell_2 \ell_n^2}{8} = \frac{0.251 \times 24 \times 18.0^2}{8} = 244 \text{ ft-kips}$$

For simplicity, use $M_o = 248.5$ ft-kips for all spans.

Division of the total panel moment M_o into negative and positive moments, and then column and middle strip moments, involves the direct application of the moment coefficients in Table 4-2.

Two-Way Slabs

Slab Moments (ft-kips)	End Spans			Int. Span
	Ext. neg.	Positive	Int. neg.	Positive
Total Moment	64.6	129.2	173.9	87.0
Column Strip	64.6	77.0	131.7	52.2
Middle Strip	0	52.2	42.2	34.8

Note: All negative moments are at face of support.

Required slab reinforcement.

Span Location		M_u (ft-kips)	b^* (in.)	d^{**} (in.)	A_s^\dagger (in. ²)	Min. A_s^\ddagger (in. ²)	Reinforcement ⁺
End Span							
Column Strip	Ext. neg.	64.6	120	7.75	2.08	1.94	11-No. 4
	Positive	77.0	120	7.75	2.48	1.94	13-No. 4
	Int. Neg.	131.7	120	7.75	4.25	1.94	22-No. 4
Middle Strip	Ext. neg.	0.0	168	7.75	---	2.72	14-No. 4
	Positive	52.2	168	7.75	1.68	2.72	14-No. 4
	Int. Neg.	42.2	168	7.75	1.36	2.72	14-No. 4
Interior Span							
Column Strip	Positive	52.2	120	7.75	1.68	1.94	10-No. 4
Middle Strip	Positive	34.8	168	7.75	1.12	2.72	14-No. 4

*Column strip width $b = (20 \times 12)/2 = 120$ in.

*Middle strip width $b = (24 \times 12) - 120 = 168$ in.

**Use average $d = 9 - 1.25 = 7.75$ in.

$\dagger A_s = M_u / 4d$ where M_u is in ft-kips and d is in inches

\ddagger Min. $A_s = 0.0018bh = 0.0162b$; Max. $s = 2h = 18$ in. or 18 in. (Sect. 13.3.2)

⁺For maximum spacing: $120/18 = 6.7$ spaces, say 8 bars

$168/18 = 9.3$ spaces, say 11 bars

Design for Shear

Check slab shear and flexural strength at edge column due to direct shear and unbalanced moment transfer.

Check slab reinforcement at exterior column for moment transfer between slab and column.

Portion of total unbalanced moment transferred by flexure = $\gamma_f M_u$

$$b_1 = 20 + (7.75/2) = 23.875 \text{ in.}$$

$$b_2 = 20 + 7.75 = 27.75 \text{ in.}$$

$$b_1 / b_2 = 0.86$$

From Fig. 4-16, $\gamma_f = 0.62^*$

*The provisions of Sect. 13.5.3.3 may be utilized; however, they are not in this example.

Two-Way Slabs

$$\gamma_f M_u = 0.62 \times 64.6 = 40 \text{ ft-kips}$$

$$\text{Required } A_s = 40 / (4 \times 7.75) = 1.29 \text{ in.}^2$$

$$\text{Number of No. 4 bars} = 1.29 / 0.2 = 6.5, \text{ say 7 bars}$$

Must provide 7-No. 4 bars within an effective slab width = $3h + c_2 = (3 \times 9) + 20 = 47 \text{ in.}$

Provide the required 7-No. 4 bars by concentrating 7 of the column strip bars (11-No. 4) within the 47 in. slab width over the column.

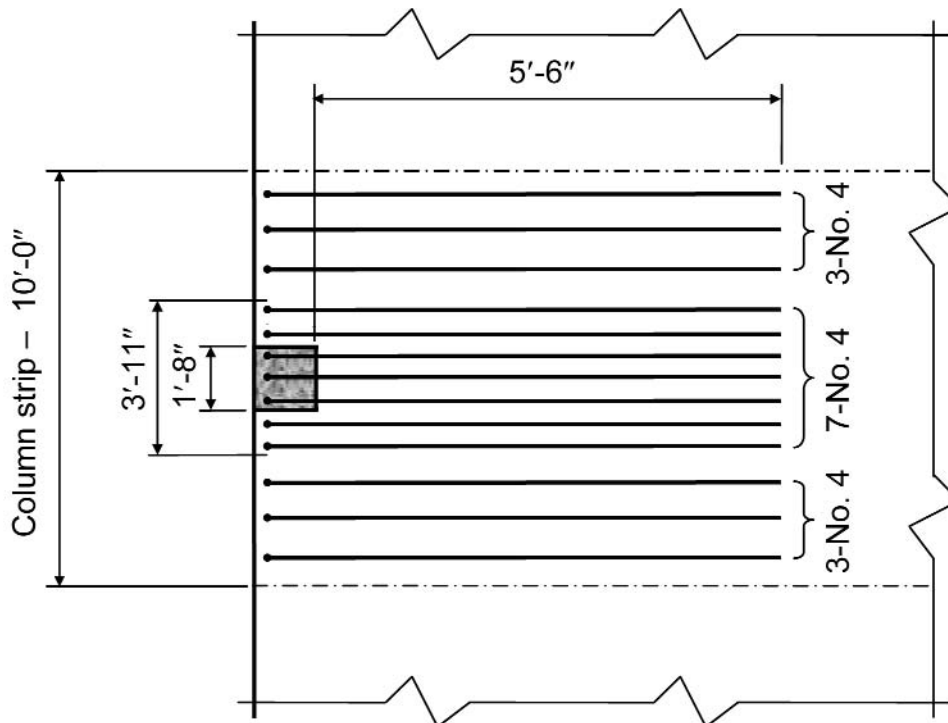
Check bar spacing:

For 7-No. 4 within 47 in. width: $47 / 7 = 6.7 \text{ in.} < 18 \text{ in. O.K.}$

For 4-No. 4 within $120 - 47 = 73 \text{ in.}$ width: $73 / 4 = 18.25 \text{ in.} > 18 \text{ in.}$

Add 1 additional bar on each side of the 47 in. strip; the spacing becomes $73 / 6 = 12.2 \text{ in.} < 18 \text{ in. O.K.}$

Reinforcement details at this location are shown in the figure on the next page.



Check the combined shear stress at the inside face of the critical transfer section.

Two-Way Slabs

$$v_u = \frac{V_u}{A_c} + \frac{\gamma_v M_u}{J/c}$$

Factored shear force at edge column:

$$\begin{aligned} V_u &= 0.251[(24 \times 10.83) - (1.99 \times 2.31)] \\ &= 64.1 \text{ kips} \end{aligned}$$

When the end span moments are determined from the Direct Design Method, the fraction of unbalanced moment transferred by eccentricity of shear must be $0.3M_o = 0.3 \times 248.5 = 74.6$ ft-kips (Sect. 13.6.3.6).

$$\gamma_v = 1 - \gamma_f = 1 - 0.62 = 0.38$$

$$c_2 / c_1 = 1.0$$

$$c_1 / d = 20/7.75 = 2.58$$

From Table 4.9

$$A_c = (2b_1 + b_2) d = 585.1 \text{ in.}^2$$

$$J_c = [2b_1 d(b_1 + 2b_2) + d^3(2b_1 + b_2)/b_1]/6 = 5,141 \text{ in.}^3$$

$$v_u = \frac{64,105}{585.1} + \frac{0.38 \times 64.6 \times 12,000}{5,141}$$

$$v_u = 109.6 + 57.6 = 167.2 \text{ psi}$$

Determine allowable shear stress ϕv_c from Fig. 4-13:

$$b_o / d = (2b_1 + b_2) / d$$

$$b_o / d = [(2 \times 23.875) + 27.75] / 7.75 = 9.74$$

$$\beta_c = 1$$

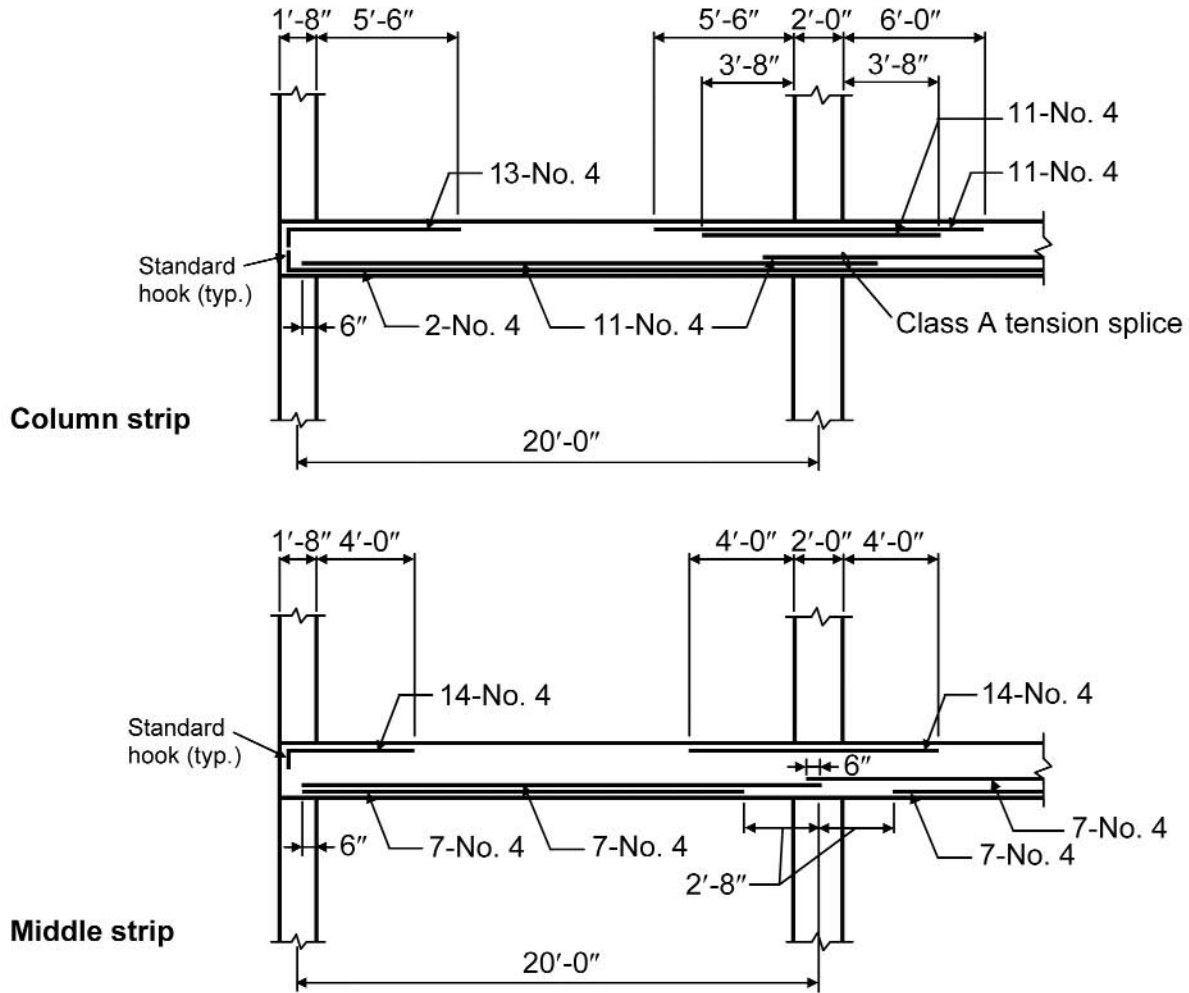
$$\phi v_c = 189.7 \text{ psi} > v_u = 168.2 \text{ psi OK}$$

9" slab is OK

Reinforcement Details

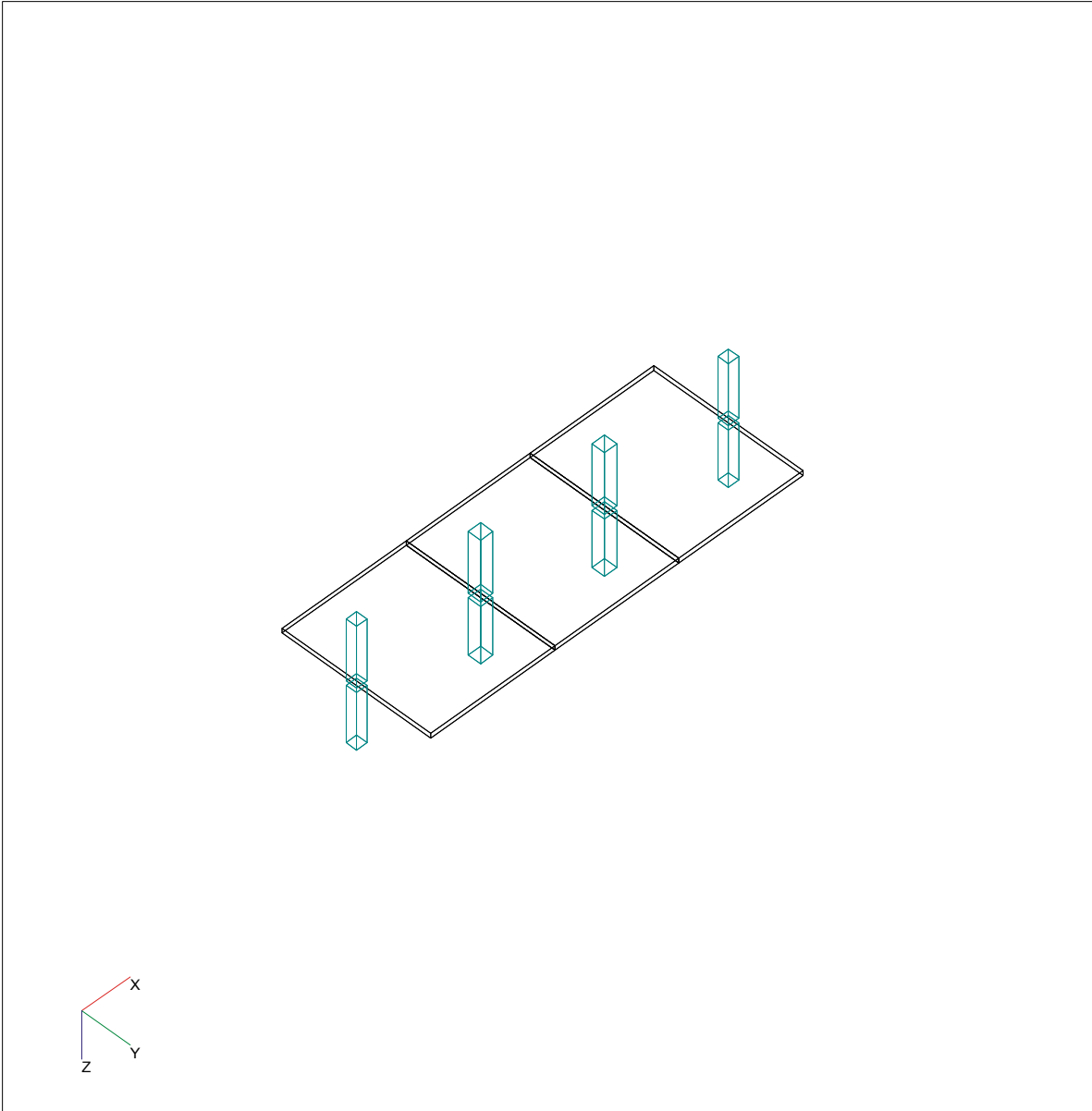
The figures below show the reinforcement details for the column and middle strips. The bar lengths are determined from Fig. 13.3.8 of ACI 318-05.

Two-Way Slabs



The PCA computer program *pcaSlab* can be used to expedite the design of different slab systems. The program covers wide range of two-way slab systems and can be used for more complex slab layouts. The output of the program for the slab in the example is shown in the following pages. Please note that the Equivalent Frame Method is used by the *pcaSlab* program.

Two-Way Slabs



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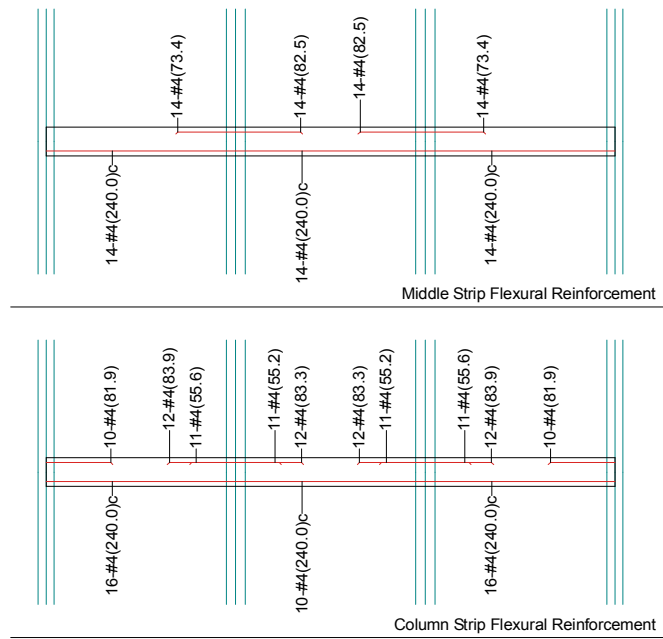
File: C:\Data\Time Saving Design Aid\Two-Way Slabs.slb

Project: Time Saving Design Aids

Frame: Two-Way Slab

Engineer: PCA

Two-Way Slabs



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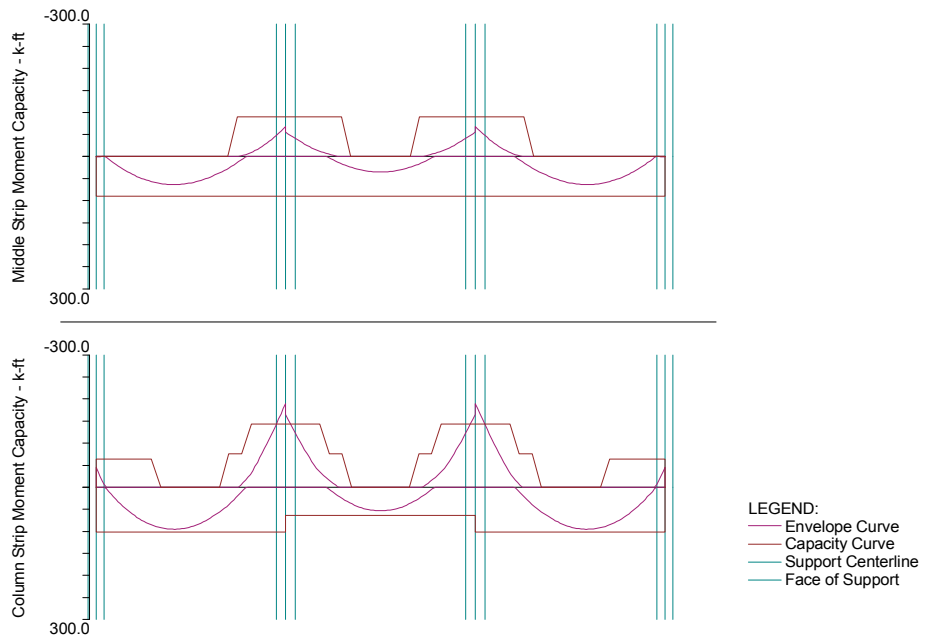
File: C:\Data\Time Saving Design Aid\Two-Way Slabs.slb

Project: Time Saving Design Aids

Frame: Two-Way Slab

Engineer: PCA

Two-Way Slabs



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File: C:\Data\Time Saving Design Aid\Two-Way Slabs.slb

Project: Time Saving Design Aids

Frame: Two-Way Slab

Engineer: PCA

Two-Way Slabs



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Page 1

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=====
                          pcaSlab v2.00 (TM)
    A Computer Program for Analysis, Design, and Investigation of
    Reinforced Concrete Beams, One-way and Two-way Slab Systems
=====
    Copyright © 2003-2006, Portland Cement Association
    All rights reserved
    
```

Licensee stated above acknowledges that Portland Cement Association (PCA) is not and cannot be responsible for either the accuracy or adequacy of the material supplied as input for processing by the pcaSlab computer program. Furthermore, PCA neither makes any warranty expressed nor implied with respect to the correctness of the output prepared by the pcaSlab program. Although PCA has endeavored to produce pcaSlab error free the program is not and cannot be certified infallible. The final and only responsibility for analysis, design and engineering documents is the licensees. Accordingly, PCA disclaims all responsibility in contract, negligence or other tort for any analysis, design or engineering documents prepared in connection with the use of the pcaSlab program.

```

=====
[1] INPUT ECHO
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General Information:

```

=====
File name: c:\Work\Time Saving Design Aids\318-05\Rev 2\Data\Two-Way Slabs.slb
Project: Time Saving Design Aids
Frame: Two-Way Slab
Engineer: PCA
Code: ACI 318-02
Reinforcement Database: ASTM A615
Mode: Design
Number of supports = 4
Floor System: Two-Way

Live load pattern ratio = 75%
Minimum free edge for punching shear = 10 times slab thickness
Deflections are based on cracked section properties.
In negative moment regions, Ig and Mcr DO NOT include flange/slab contribution (if available)
Long-term deflections are calculated for load duration of 60 months.
0% of live load is sustained.
Compression reinforcement calculations NOT selected.
    
```

Material Properties:

```

=====
                Slabs|Beams          Columns
                -----
wc  =          150          150 lb/ft3
f'c =           4           4 ksi
Ec  =        3834.3        3834.3 ksi
fr  =         0.47434        0.47434 ksi

fy  =          60 ksi, Bars are not epoxy-coated
fyv =          60 ksi
Es  =        29000 ksi
    
```

Reinforcement Database:

```

=====
Units: Db (in), Ab (in^2), Wb (lb/ft)
Size  Db    Ab    Wb    Size  Db    Ab    Wb
-----
    
```

Two-Way Slabs



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#3	0.38	0.11	0.38	#4	0.50	0.20	0.67
#5	0.63	0.31	1.04	#6	0.75	0.44	1.50
#7	0.88	0.60	2.04	#8	1.00	0.79	2.67
#9	1.13	1.00	3.40	#10	1.27	1.27	4.30
#11	1.41	1.56	5.31	#14	1.69	2.25	7.65
#18	2.26	4.00	13.60				

Span Data:

=====
 Slabs: L1, wL, wR (ft); t, Hmin (in)
 Span Loc L1 t wL wR Hmin

1 Int	20.000	9.00	12.000	12.000	7.27
2 Int	20.000	9.00	12.000	12.000	6.55
3 Int	20.000	9.00	12.000	12.000	7.27

Support Data:

=====
 Columns: c1a, c2a, c1b, c2b (in); Ha, Hb (ft)
 Supp c1a c2a c1b c2b Ha Hb Red%

1	20.00	20.00	10.000	20.00	20.00	10.000	100
2	24.00	24.00	10.000	24.00	24.00	10.000	100
3	24.00	24.00	10.000	24.00	24.00	10.000	100
4	20.00	20.00	10.000	20.00	20.00	10.000	100

Boundary Conditions: Kz (kip/in); Kry (kip-in/rad)

Supp Spring Kz Spring Kry Far End A Far End B

1	0	0	Fixed	Fixed
2	0	0	Fixed	Fixed
3	0	0	Fixed	Fixed
4	0	0	Fixed	Fixed

Load Data:

=====
 Load Cases and Combinations:

Case	SELF	Dead	Live
Type	DEAD	DEAD	LIVE
U1	1.400	1.400	0.000
U2	1.200	1.200	1.600
U3	1.200	1.200	1.600
U4	1.200	1.200	1.600
U5	1.200	1.200	1.000
U6	1.200	1.200	1.000
U7	0.900	0.900	0.000
U8	0.900	0.900	0.000
U9	1.200	1.200	1.000
U10	1.200	1.200	1.000
U11	0.900	0.900	0.000
U12	0.900	0.900	0.000

Span Loads:

Span Case Wa

 Area Loads - Wa (lb/ft2):

1 Dead	30
2 Dead	30
3 Dead	30
1 Live	50
2 Live	50
3 Live	50

Support Loads - Fz (kip), My (k-ft):

Supp Case Fz My

1 SELF	0	0
2 SELF	0	0
3 SELF	0	0
4 SELF	0	0
1 Live	0	0
2 Live	0	0
3 Live	0	0
4 Live	0	0

Support Displacements - D (in), R (rad):

Supp Case D R

1 SELF	0	0
2 SELF	0	0
3 SELF	0	0
4 SELF	0	0
1 Live	0	0
2 Live	0	0
3 Live	0	0
4 Live	0	0



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Reinforcement Criteria:

	Top bars		Bottom bars		Stirrups	
	Min	Max	Min	Max	Min	Max
Slabs and Ribs:						
Bar Size	#4	#8	#4	#8		
Bar spacing	1.00	18.00	1.00	18.00	in	
Reinf ratio	0.14	5.00	0.14	5.00	%	
Cover	1.50		1.50		in	
Beams:						
Bar Size	#5	#8	#5	#8	#3	#5
Bar spacing	1.00	18.00	1.00	18.00	6.00	18.00
Reinf ratio	0.14	5.00	0.14	5.00	%	
Cover	1.50		1.50		in	
Side cover	1.50		1.50		in	
Layer dist.	1.00		1.00		in	
No. of legs					2	6

[2] DESIGN RESULTS*

*Unless otherwise noted, all results are in the direction of analysis only. Another analysis in the perpendicular direction has to be carried out for two-way slab systems.

Top Reinforcement:

Units: Width (ft), Mmax (k-ft), Xmax (ft), As (in^2), Sp (in)

Span Strip	Zone	Width	Mmax	Xmax	AsMin	AsMax	SpReq	AsReq	Bars	
1 Column	Left	10.00	6.22	0.833	1.944	15.714	12.000	0.191	10-#4	
	Middle	10.00	0.00	9.917	0.000	15.714	0.000	0.000	---	
	Right	10.00	142.72	19.000	1.944	15.714	5.217	4.588	23-#4	
	Middle	Left	14.00	-0.00	0.833	0.000	22.000	0.000	0.000	---
	Middle	Middle	14.00	0.00	9.917	0.000	22.000	0.000	0.000	---
	Middle	Right	14.00	47.58	19.000	2.722	22.000	12.000	1.474	14-#4
2 Column	Left	10.00	122.98	1.000	1.944	15.714	5.217	3.926	23-#4	
	Middle	10.00	0.00	10.000	0.000	15.714	0.000	0.000	---	
	Right	10.00	122.98	19.000	1.944	15.714	5.217	3.926	23-#4	
	Middle	Left	14.00	40.99	1.000	2.722	22.000	12.000	1.268	14-#4
	Middle	Middle	14.00	0.00	10.000	0.000	22.000	0.000	0.000	---
	Middle	Right	14.00	40.99	19.000	2.722	22.000	12.000	1.268	14-#4
3 Column	Left	10.00	142.72	1.000	1.944	15.714	5.217	4.588	23-#4	
	Middle	10.00	0.00	10.083	0.000	15.714	0.000	0.000	---	
	Right	10.00	6.22	19.167	1.944	15.714	12.000	0.191	10-#4	
	Middle	Left	14.00	47.58	1.000	2.722	22.000	12.000	1.474	14-#4
	Middle	Middle	14.00	0.00	10.083	0.000	22.000	0.000	0.000	---
	Middle	Right	14.00	-0.00	19.167	0.000	22.000	0.000	0.000	---

Top Bar Details:

Units: Length (ft)

Span Strip	Bars	Left		Continuous		Right		Bars	Length
		Length	Bars	Length	Bars	Length	Bars		
1 Column	10-#4	6.83	---	---	---	12-#4	7.00	11-#4	4.63
	Middle	---	---	---	---	14-#4	6.12	---	---
2 Column	12-#4	6.94	11-#4	4.60	---	12-#4	6.94	11-#4	4.60
	Middle	14-#4	6.87	---	---	14-#4	6.87	---	---
3 Column	12-#4	7.00	11-#4	4.63	---	10-#4	6.83	---	---
	Middle	14-#4	6.12	---	---	---	---	---	---

Bottom Reinforcement:

Units: Width (ft), Mmax (k-ft), Xmax (ft), As (in^2), Sp (in)

Span Strip	Width	Mmax	Xmax	AsMin	AsMax	SpReq	AsReq	Bars
1 Column	10.00	95.59	8.299	1.944	15.714	7.500	3.023	16-#4
	Middle	14.00	63.73	8.299	2.722	22.000	12.000	1.982
2 Column	10.00	52.89	10.000	1.944	15.714	12.000	1.649	10-#4
	Middle	14.00	35.26	10.000	2.722	22.000	12.000	1.089
3 Column	10.00	95.59	11.701	1.944	15.714	7.500	3.023	16-#4
	Middle	14.00	63.73	11.701	2.722	22.000	12.000	1.982

Bottom Bar Details:



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Units: Start (ft), Length (ft)

Span	Strip	Long Bars		Short Bars	
		Bars	Start Length	Bars	Start Length
1	Column	16-#4	0.00 20.00	---	---
	Middle	14-#4	0.00 20.00	---	---
2	Column	10-#4	0.00 20.00	---	---
	Middle	14-#4	0.00 20.00	---	---
3	Column	16-#4	0.00 20.00	---	---
	Middle	14-#4	0.00 20.00	---	---

Flexural Capacity:

Units: x (ft), As (in²), PhiMn (k-ft)

Span	Strip	x	As		PhiMn-	PhiMn+
			AsTop	AsBot		
1	Column	0.000	2.00	3.20	-63.93	101.01
		0.833	2.00	3.20	-63.93	101.01
		5.829	2.00	3.20	-63.93	101.01
		6.829	0.00	3.20	0.00	101.01
		7.192	0.00	3.20	0.00	101.01
		10.000	0.00	3.20	0.00	101.01
		12.642	0.00	3.20	0.00	101.01
		13.005	0.00	3.20	0.00	101.01
		14.005	2.40	3.20	-76.39	101.01
		15.366	2.40	3.20	-76.39	101.01
	Middle	16.366	4.60	3.20	-143.07	101.01
		19.000	4.60	3.20	-143.07	101.01
		20.000	4.60	3.20	-143.07	101.01
		0.000	0.00	2.80	0.00	89.50
		0.833	0.00	2.80	0.00	89.50
		7.192	0.00	2.80	0.00	89.50
		10.000	0.00	2.80	0.00	89.50
		12.642	0.00	2.80	0.00	89.50
		13.883	0.00	2.80	0.00	89.50
		14.883	2.80	2.80	-89.50	89.50
2	Column	0.000	4.60	2.00	-143.07	63.93
		1.000	4.60	2.00	-143.07	63.93
		3.601	4.60	2.00	-143.07	63.93
		4.601	2.40	2.00	-76.39	63.93
		5.940	2.40	2.00	-76.39	63.93
		6.940	0.00	2.00	0.00	63.93
		7.300	0.00	2.00	0.00	63.93
		10.000	0.00	2.00	0.00	63.93
		12.700	0.00	2.00	0.00	63.93
		13.060	0.00	2.00	0.00	63.93
	Middle	14.060	2.40	2.00	-76.39	63.93
		15.399	2.40	2.00	-76.39	63.93
		16.399	4.60	2.00	-143.07	63.93
		19.000	4.60	2.00	-143.07	63.93
		20.000	4.60	2.00	-143.07	63.93
		0.000	2.80	2.80	-89.50	89.50
		1.000	2.80	2.80	-89.50	89.50
		5.875	2.80	2.80	-89.50	89.50
		6.875	0.00	2.80	0.00	89.50
		7.300	0.00	2.80	0.00	89.50
3	Column	0.000	4.60	3.20	-143.07	101.01
		1.000	4.60	3.20	-143.07	101.01
		3.634	4.60	3.20	-143.07	101.01
		4.634	2.40	3.20	-76.39	101.01
		5.995	2.40	3.20	-76.39	101.01
		6.995	0.00	3.20	0.00	101.01
		7.358	0.00	3.20	0.00	101.01
		10.000	0.00	3.20	0.00	101.01
		12.808	0.00	3.20	0.00	101.01
		13.171	0.00	3.20	0.00	101.01
	Middle	14.171	2.00	3.20	-63.93	101.01
		19.167	2.00	3.20	-63.93	101.01
		20.000	2.00	3.20	-63.93	101.01
		0.000	2.80	2.80	-89.50	89.50
		1.000	2.80	2.80	-89.50	89.50
		5.117	2.80	2.80	-89.50	89.50
		6.117	0.00	2.80	0.00	89.50
		7.358	0.00	2.80	0.00	89.50
		10.000	0.00	2.80	0.00	89.50



Two-Way Slabs

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	12.808	0.00	2.80	0.00	89.50
	19.167	0.00	2.80	0.00	89.50
	20.000	0.00	2.80	0.00	89.50

Slab Shear Capacity:

Units: b, d (in), Xu (ft), PhiVc, Vu(kip)

Span	b	d	Vratio	PhiVc	Vu	Xu
1	288.00	7.25	1.000	198.09	61.26	18.40
2	288.00	7.25	1.000	198.09	50.58	18.40
3	288.00	7.25	1.000	198.09	61.26	1.60

Flexural Transfer of Negative Unbalanced Moment at Supports:

Units: Width (in), Munb (k-ft), As (in^2)

Supp	Width	Gamma*Munb	Comb	Pat	AsReq	AsProv	Additional Bars
1	47.00	30.23	U2	All	0.950	0.783	1-#4
2	51.00	33.44	U2	Odd	1.051	1.955	---
3	51.00	33.44	U2	Odd	1.051	1.955	---
4	47.00	30.23	U2	All	0.950	0.783	1-#4

Punching Shear Around Columns:

Units: Vu (kip), Munb (k-ft), vu (psi), Phi*vc (psi)

Supp	Vu	vu	Munb	Comb	Pat	GammaV	vu	Phi*vc
1	48.92	129.4	3.20	U2	All	0.320	134.6	189.7
2	129.49	149.2	-37.01	U2	All	0.400	168.7	189.7
3	129.49	149.2	37.01	U2	All	0.400	168.7	189.7
4	48.92	129.4	-3.20	U2	All	0.320	134.6	189.7

Deflections:

Section properties

Units: Ig, Icr, Ie (in^4), Mcr, Mmax (k-ft)

Span	Ie,avg			Ig	Icr	Mcr	Load Level			
	Dead	Dead+Live	Zone				Mmax	Ie	Mmax	Ie
1	17496	16272	Middle	17496	1816	153.69	90.45	17496	122.19	17496
			Right	17496	2174	153.69	-146.59	17496	-198.03	9336
2	17496	16317	Left	17496	2174	153.69	-125.58	17496	-169.64	13567
			Middle	17496	1494	153.69	45.42	17496	61.36	17496
			Right	17496	2174	153.69	-125.58	17496	-169.64	13567
3	17496	16272	Left	17496	2174	153.69	-146.59	17496	-198.03	9336
			Middle	17496	1816	153.69	90.45	17496	122.19	17496

Maximum Instantaneous Deflections - Direction of Analysis

Units: D (in), Ig (in^4)

Span	Frame			Ig	LDF	Strips Ratio	D			
	Ddead	Dlive	Dtotal				Ddead	Dlive	Dtotal	
1	0.074	0.032	0.106	Column	7290	0.738	1.770	0.132	0.056	0.188
				Middle	10206	0.262	0.450	0.034	0.014	0.048
2	0.022	0.009	0.031	Column	7290	0.675	1.620	0.036	0.015	0.051
				Middle	10206	0.325	0.557	0.012	0.005	0.017
3	0.074	0.032	0.106	Column	7290	0.738	1.770	0.132	0.056	0.188
				Middle	10206	0.262	0.450	0.034	0.014	0.048

Maximum Long-term Deflections - Direction of Analysis

Time dependant factor for sustained loads = 2.000

Units: D (in)

Span	Column		Strip		Dtotal	Middle		Strip		Dtotal		
	Dsust	Lambda	Dcs	Dcs+lu		Dcs	Dcs+lu	Dcs+1	Dtotal			
1	0.132	2.000	0.264	0.320	0.320	0.451	0.034	2.000	0.067	0.081	0.081	0.115
2	0.036	2.000	0.071	0.086	0.086	0.122	0.012	2.000	0.024	0.030	0.030	0.042
3	0.132	2.000	0.264	0.320	0.320	0.451	0.034	2.000	0.067	0.081	0.081	0.115

Material Takeoff:

Reinforcement in the Direction of Analysis

Top Bars:	693.4 lb	<=>	11.56 lb/ft	<=>	0.481 lb/ft^2
Bottom Bars:	1122.2 lb	<=>	18.70 lb/ft	<=>	0.779 lb/ft^2
Stirrups:	0.0 lb	<=>	0.00 lb/ft	<=>	0.000 lb/ft^2
Total Steel:	1815.6 lb	<=>	30.26 lb/ft	<=>	1.261 lb/ft^2
Concrete:	1080.0 ft^3	<=>	18.00 ft^3/ft	<=>	0.750 ft^3/ft^2